

EN 1998-5:2020 - Section 11: Underground Structures

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11 UNDERGROUND STRUCTURES

- New section in EN 1998-5
- The section is limited to the **determination of action effects on underground structures**
- It does not cover design verifications!



11 UNDERGROUND STRUCTURES

• Structure / Contents:

11.1 General

11.2 Seismic actions

- 11.2.1 General requirements
- 11.2.2 Ground motion parameters
- 11.2.3 Permanent ground displacement parameters

11.3 Methods of analysis

- 11.3.1 Seismic action for underground structures
- 11.3.2 Transient seismic action
- 11.3.3 Permanent ground deformation

11.4 Seismic loading for large underground spaces (parking and metro stations)

- 11.4.1 Ground shaking
- 11.4.2 Permanent ground displacements

11.5 Culverts



11 UNDERGROUND STRUCTURES

Associated Annexes

Annex G (Informative) Simplified evaluation of peak ground motion parameters for seismic design of underground structures

Annex H (Informative) Simplified analytical expressions for the seismic design of tunnels

Annex I (Informative) Impedance functions for underground structures



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- (1) P Tunnels (bored, cut and cover, immersed) and underground structures (culverts and underground large works, like metro and parking stations, pipelines) shall be designed to provide seismic performance consistent with the limit states defined in EN 1998-1–1:2019, 4.4.1(1), EN 1998-3:2019, 4.1(2), and the associated seismic actions
- (2) P Underground structures shall be designed against:

ground shaking

permanent ground deformations due to seismic fault crossing, seismically induced landslides and liquefaction induced phenomena



• (3) Tunnels and other underground structures should **primarily be designed** to accommodate the **transient and permanent deformations**

Why? The imposed ground deformations (transient and permanent) on underground structures are more important than transient seismic loads related to the structure's inertia

• (4) Spatially extended underground structures: seismic design in the transverse and longitudinal direction should consider the spatial variability of the ground motion and the associated phenomena



• (5) Soil-structure-interaction effects should be considered according to the general rules in § 8, complemented with the provisions of § 11.3

• (6) Seismic earth pressures may be estimated according to § 10.3, and duly adjusted with the provisions of § 11.3



11.2 SEISMIC ACTIONS

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11.2.1 GENERAL REQUIREMENTS

• (1) Estimation of seismic actions due to ground shaking

Acc. to EN1998-1-1:2019 after adjustment accounting for the **depth** and **dimensions** of the underground structure and the **spatial variability** of ground motion

Annex A provides guidance on the estimation of ground motion



11.2.1 GENERAL REQUIREMENTS

• (2) Underground structures crossing potentially active faults

Potentially active faults defined as in § 7.1.2

Necessary parameters that should be estimated are the **angle of incidence**, **dip and offset at the location of the structure**

• (3) Effects by precarious slopes on tunnels/culverts

Specific ground response and slope stability analyses should be carried out to estimate the type and magnitude of **permanent slope displacements** in the seismic design situation, according to § 7.2



11.2.1 GENERAL REQUIREMENTS

• (4) Underground structures in **potentially liquefiable soils**

Specific ground response and liquefaction assessment should be carried out, according to § 7.5 and § 7.3, aimed at estimating the spatial variability of liquefaction and the severity of **buoyancy effects**

• (5) Sites susceptible to hazards such as active faults, precarious slopes and potentially liquefiable soils should be avoided, unless specific design and construction actions reduce the risk to acceptable limits!



- (1) Ground motion parameters should be established for the seismic design of tunnels and underground structures
- (2) Low and moderate seismic action classes → peak ground motion parameters PGA, PGV, PGD may be used

Design response spectra should be consistent with these parameters

(3) For the evaluation of parameters at ground surface, various depths of the embedded structure, and at the depth of the base of the underground structure:
A ground-specific response analysis may be carried out for this purpose



- (4) Moderate and high seismic action classes → a ground-specific response analysis should be carried out along the total length of the structure
- (5) For low seismic action classes and in the absence of site-specific ground response analysis, the ground motion parameters at depth z in clauses (1) and (2) may be calculated from PGA at ground surface, (e.g., EN 1998–1–1:2019, 5.2.2.4) using simplified expressions
- (6) In the absence of site-specific response analysis the values of PGV(z) and PGD(z) may be estimated using empirical correlations

Annex G provides simplified expressions and empirical relations

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- Annex G provides:
 - Simplified relations to estimate **PGA** distribution with depth
 - Empirical correlations between PGA, PGV and PGD
 - Formulae to estimate ground shear stresses distribution with depth
 - Recommendations for the estimation of spatial variation and incoherence of the ground motion



- (7) For the seismic action in the longitudinal direction of tunnels and pipelines, an apparent velocity (V_{app}) should be considered.
- (8) Absence of site-specific studies? V_{app} may be taken equal to 1000 m/s



11.2.2 PERMANENT GROUND DISPLACEMENT PARAMETERS

- (1) For seismic faulting, seismically triggered landslides, or liquefaction, as defined in § 7.1.1, § 7.2 and § 7.3, the permanent ground displacements should be calculated together with other relevant design parameters for the design return period and the category of structures under consideration
- (2) For permanent ground displacements not covered in (1), specific studies should be performed



11.3 METHODS OF ANALYSIS

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11.3.1 SEISMIC ACTION FOR UNDERGROUND STRUCTURES

• (1) For the seismic design of underground structures, the **transient effect of the** seismic action may be expressed in terms of:

a) Forces in the transverse direction (as per § 11.3.2.1)

b) Ground deformations in both transverse and longitudinal directions (as per §11.3.2.2)

• (2) The effect of seismic action due to **permanent ground deformation** should be expressed in terms of **displacements** (as per § 11.3.3)



11.3.2 TRANSIENT SEISMIC ACTION

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11.3.2.1 FORCES IN THE TRANSVERSE DIRECTION

(1) Estimation of seismic earth pressures acting on the structures in the transverse direction? → methods as per clauses of § 10.3 may be used

• IMPORTANT NOTE!

- Methods as in § 10.3 are appropriate for shallow tunnels, culverts and other underground mainly cut-and cover structures
- For **deep** tunnels and undergrounds structures, like metro and parking stations, this approach involves **uncertainties** and the method in § 11.3.2.2 is preferred



• (1) Analysis methods should be based on the main dynamic response patterns due to the seismic ground excitation and wave propagation

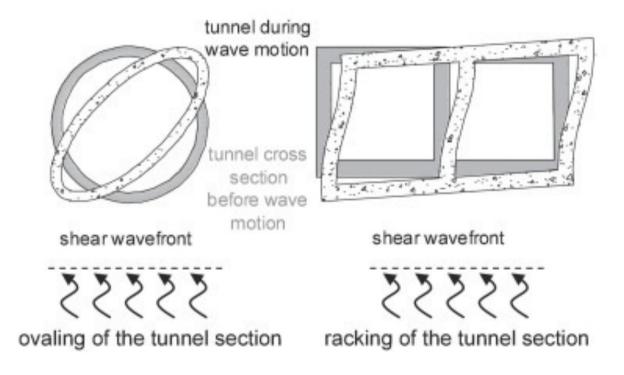
Two **main deformation modes** should be considered for **transverse response** of tunnels, in a) or b) as appropriate:

a) Ovaling response in circular or horse-shoe type tunnels

b) Racking-rocking response in rectangular cut-and-cover tunnels



• Main deformation modes for transverse response of tunnels



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• (2) How to determine the response due to seismic deformation in transverse direction ? Use of:

Closed form analytical solutions, with or without consideration of soil-structure interaction effects

Advanced numerical methods (preferable for high seismic action classes)

Annex H provides expressions for the closed form solutions



 (3), (4) Analysis when soil-structure interaction is ignored → it may be assumed that free-field ground shear deformations along the depth of the tunnel are directly applied statically to the lining to compute the seismic loadings

Annex H provides guidance for the calculations of the internal forces



• (5), (6) Analysis when soil-structure-interaction effects are considered \rightarrow

In cases of **circular tunnels**, simplified analytical expressions accounting for the **relative flexibility of the structure and the soil** may be used

Annex H provides such simplified analytical expressions

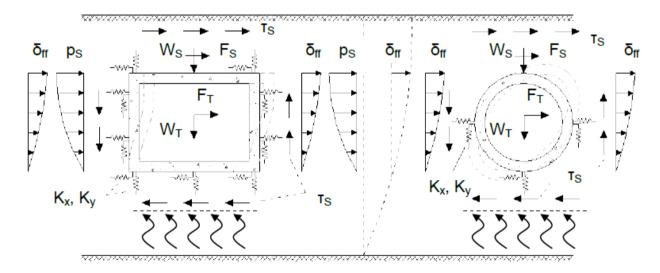
In cases of **cut-and-cover rectangular tunnels**, the seismic analysis may be based on methods accounting for the **flexibility ratio of the tunnel to the surrounding ground**

Annex H provides guidance on these methods

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 (7) When soil-structure interaction effects are considered for the seismic analysis in the transverse direction, the model may follow § 8.3 using springs (normal and tangential) consistent with the vibration modes and the dominating deformation pattern





• (8) Springs stiffnesses in (7) should depend on the soil type where the underground structure is embedded, the type of the underground structure, the deformation modes, the seismic strain amplitude for the design ground shaking and the soil strength limit states

Annex I provides guidance for the calculations of the springs stiffnesses



• (9) For the seismic analysis in the longitudinal direction of tunnels and other long underground structures, when soil-structure interaction effects are neglected, the analysis may assume that the longitudinal strains in the tunnel are equal to the ground motion strains in the free-field due to the passage of seismic waves

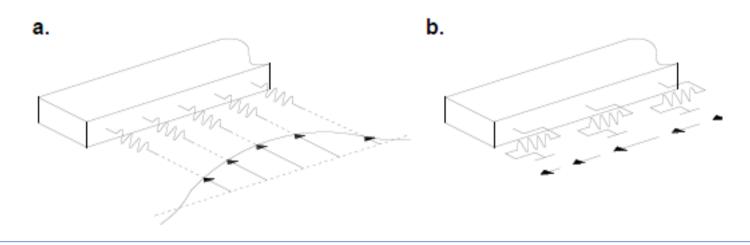
Annex H provides guidance for the calculations of the strains



- To sum up, Annex H provides:
 - Simplified relations for the computation of deformations and lining forces of circular tunnels subjected to ground shaking in the transverse direction, when considering or neglecting SSI phenomena
 - Simplified methods for the computation of deformations and lining forces of rectangular underground structures subjected to ground shaking in the transverse direction, when considering SSI phenomena
 - Simplified relations for the computation of deformations and lining forces of tunnels and underground structures subjected to ground shaking in the longitudinal direction, when considering or neglecting SSI phenomena



• (10) For the seismic analysis in the longitudinal direction of long underground structures, when soil-structure interaction effects are accounted for, the analysis may be based on the Beam-on-Dynamic-Winkler foundation approach with selection of the values of springs and dashpots to simulate the shear (tangential) and normal soil-structure interaction



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• Annex I provides guidance for the calculations of the springs and dashpots

- Soil-structure-interaction effects in the longitudinal direction generally reduce the internal forces in the lining
- The reduction for ordinary ratios of soil to structure stiffness is relatively small



- The greatest risk to underground structures is the potential for large ground movements as a result of fault crossing, landslides and liquefaction hazards
- In general, it is not easy to design underground structures to withstand large permanent ground displacements!
- A preferred strategy is to avoid any potential site susceptible to these hazards!



 (1) Estimation of permanent ground displacements for landslide and liquefaction hazards?

Acc. to § 7.2.2.3 and § 7.3.5(6) or other properly validated approaches

Empirical relationships that correlate displacements to earthquake magnitude and fault type may introduce very high uncertainties



- (2), (3) When it is impossible to avoid crossing landslide and liquefaction prone areas, ground stabilisation or appropriate design of structures to undertake potential deformations should be made
- (4) In case it cannot be verified that liquefaction will not occur in the seismic design situation, the design should account for buoyancy effects
- (5) Analysis of tunnels against **dip slip faulting (normal and reverse)**, perpendicular to the tunnel axis may be based on a procedure analysis applied to pipelines

To comply with (5), different approaches may be also applied (i.e. oversize excavation, use of compressible backfill material, design and manufacture of the joints to absorb gradually the longitudinal fault displacements)



- (6) For strike slip faulting, countermeasures similar to (5) should be taken to minimize the consequences of the faulting offset
- (7), (8) Estimation of spatial distribution and attenuation of the maximum fault displacements along the tunnel axis?

via empirical relations or

numerically using appropriate 2D or 3D numerical approaches simulating the ground and the fault offset geometry and mechanism (preferable for **high seismic action classes**, where the soil-segmented tunnel interaction should be adequately modelled)



- (9) To comply with (5), the joints of segmented lining should be able to
 accommodate the permanent ground displacements along the tunnel axis and on
 both sides of the faulting zone
- Joints having special design features and capacities should be used in case of large fault displacements
- NOTE For fault displacements exceeding 800 mm-1000 mm, it can be difficult to structurally accommodate the imposed ground displacements using specially designed joints, and other solutions need to be investigated and implemented!
- (10) Similar approaches to (7) should also be applied in case of excessive permanent displacements caused by landslides and liquefaction

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11.4 SEISMIC LOADING FOR LARGE UNDERGROUND SPACES



• (1) Analysis of large underground structures (e.g. parking garage, metro stations)?

Analysis accounting explicitly for structure and ground response, including soilstructure interaction effects

 (2) Pseudo static analysis, as per § 10.3.2, where the underground structure is modelled as frame structure subjected to static and dynamic earth pressures, should not be used unless both a) and b) apply:

a) the distribution of total earth pressures (static and dynamic) with depth satisfies the hypotheses of § 10.3.2

b) the underground structure has a limited depth, in order to fulfil the conditions for the development of earthquake earth pressures according to § 10.3.2

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- (3) Large underground structures subjected to seismic shaking may be analyzed using a two-dimensional (2D) frame-spring model
- Annex I provides specifications for such an analysis
- (4) The seismic loads may be introduced statically, applying an equivalent inertial force induced by the maximum ground acceleration or equivalent ground displacement at the individual springs, both calculated under free-field conditions from a site response analysis
- Annex I provides guidance for approximate estimates of strain compatible soil springs



 Annex I provides guidance for approximate estimates of strain compatible soil springs

These estimates can only be **used for rather shallow structures** with depth not exceeding 10-15 m

For deeper structures, the use of spring expressions provided in Annex I can lead to large uncertainties and differences in the calculated internal forces



• (5) For underground structures in high seismic action classes, full dynamic time history 2D or 3D analysis of the coupled soil-structure system

Ground and structure properties should be simulated in a wide range of strains



11.4.2 PERMANENT GROUND DISPLACEMENTS

- Large underground structures can not accommodate moderate to large permanent ground displacements due to seismic fault failure
- Best strategy for seismic design is to relocate these structures far from the fault offset
- (1) For very stiff structures crossing a fault, § 7.1.2 may be applied



11.5 CULVERTS

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11.5 CULVERTS

- Typical structures (rigid-flexible) in transportation and hydraulic networks generally of short length and dimensions
- Consider the seismic response of the ground, the embankment and earth fill in which they are embedded
- Culverts are particularly vulnerable to permanent ground deformations!
- Effects of transient ground shaking may be neglected for culverts, of any shape and typology, with less than 2,0 m span and may be designed according to § 11.1 to § 11.3 for large dimension culverts
- Design of joints of segmental culverts: Provide enough deformation capacity in tension and compression to withstand transient and permanent longitudinal ground displacements

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